

# Electrical, Electronic and Digital Principles (EEDP)

## Lecture 5

CE Amplifier, Coupling,  
and Multistage Amplifiers

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# 6-3 THE COMMON-EMITTER AMPLIFIER

## Total Output Resistance

➤ The output resistance of any system is defined as the resistance  $R_o$  ( $Z_o$ ) determined when  $V_i = 0$ .

when  $V_i = 0$ ,  $I_i = I_b = 0$ , resulting in an open-circuit equivalence for the current source.

$$Z_o = R_C \parallel r_o$$

If  $r_o \geq 10R_C$ , the approximation  $R_C \parallel r_o \cong R_C$  is frequently applied, and

$$Z_o \cong R_C$$

$$r_o \geq 10R_C$$

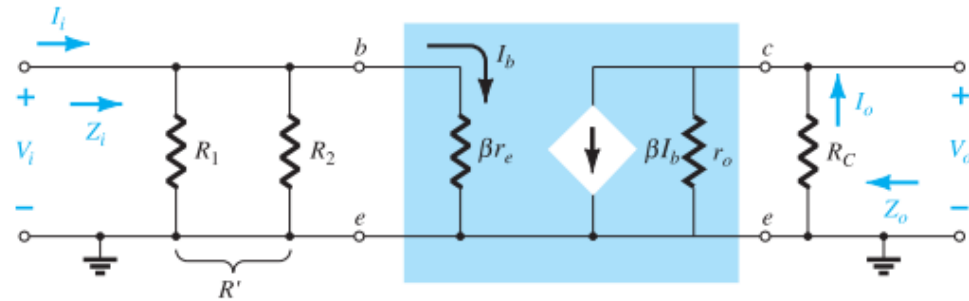
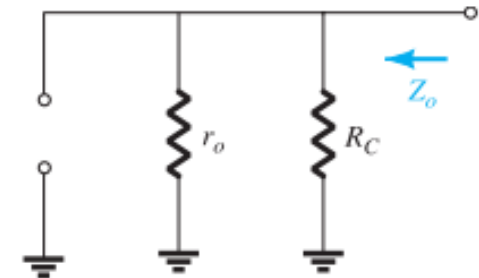


FIG. 5.27

Substituting the  $r_e$  equivalent circuit into the ac equivalent network of Fig. 5.26.



# Voltage Gain

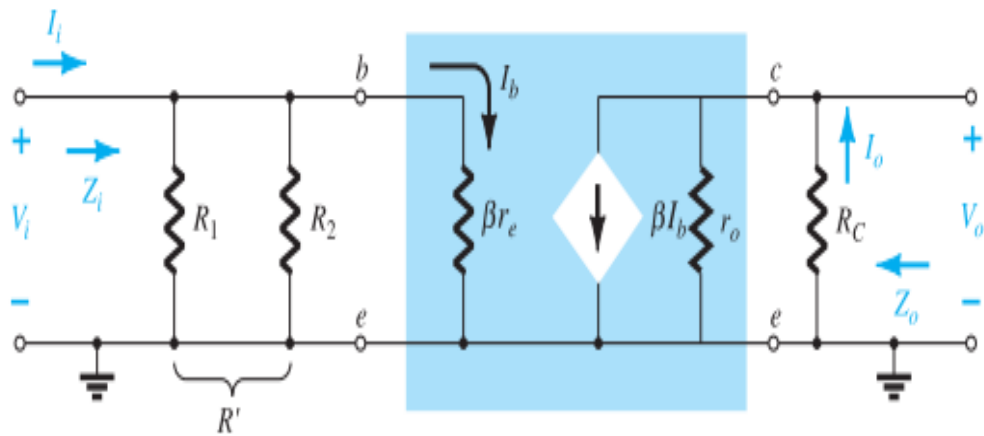
The gain is the ratio of ac output voltage at the collector ( $V_c$ ) to ac input voltage at the base ( $V_b$ ).

$$V_o = -(\beta I_b)(R_C \parallel r_o)$$

$$I_b = \frac{V_i}{\beta r_e}$$

$$V_o = -\beta \left( \frac{V_i}{\beta r_e} \right) (R_C \parallel r_o)$$

$$\frac{V_c}{V_b}$$



the voltage gain from base to collector.

$$A_v = \frac{V_o}{V_i} = \frac{-R_C \parallel r_o}{r_e}$$

**Phase Relationship** The negative sign of Eq. (5.15) reveals a  $180^\circ$  phase shift between  $V_o$  and  $V_i$ .

For  $r_o \geq 10R_C$ ,

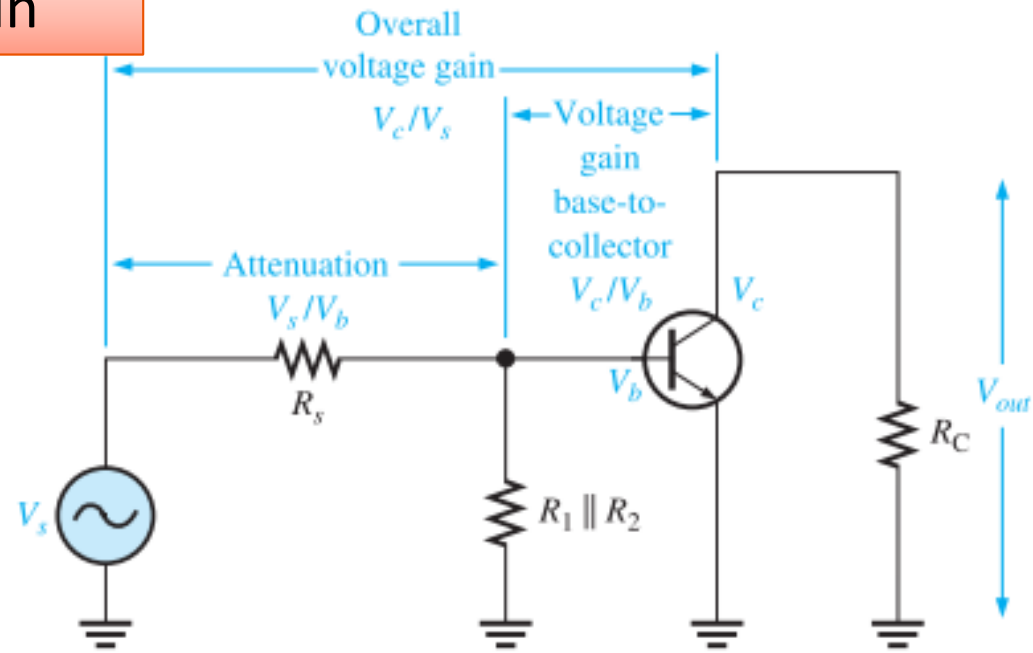
$$A_v = \frac{V_o}{V_i} \cong -\frac{R_C}{r_e}$$

$r_o \geq 10R_C$

To get the overall gain of the amplifier from the source voltage to collector, the attenuation of the input circuit must be included

## Attenuation and the Overall Gain

$$\text{Attenuation} = \frac{V_s}{V_b} = \frac{R_s + R_{in(tot)}}{R_{in(tot)}}$$



## Overall Voltage Gain

$$A'_v = \left( \frac{V_c}{V_b} \right) \left( \frac{V_b}{V_s} \right) = \frac{V_c}{V_s}$$

## Effect of a Load on the Voltage Gain

When a resistor,  $R_L$ , is connected to the output through the coupling capacitor  $C_3$ , as shown in Figure 6–17(a), it creates a load on the circuit.

$$R_c = \frac{R_C R_L}{R_C + R_L}$$

Replacing  $R_C$  with  $R_c$  in the voltage gain expression gives

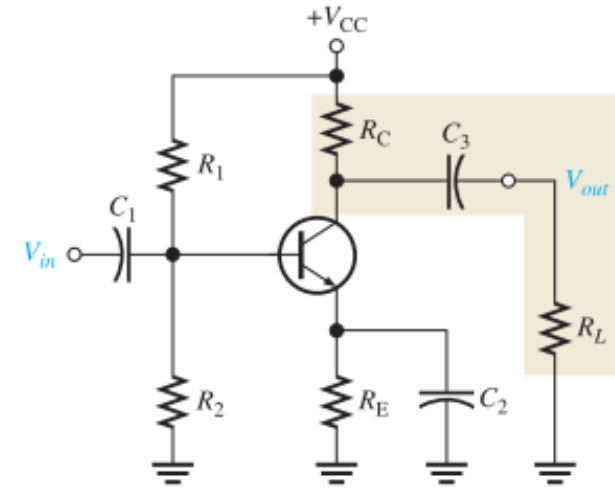
$$A_v = \frac{R_c}{r'_e}$$

When  $R_c < R_C$  because of  $R_L$ , the voltage gain is reduced.

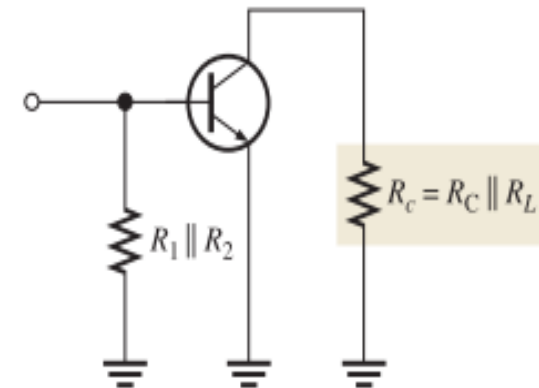
However, if  $R_L \gg R_C$  then:

$$R_c \cong R_C$$

and the load has very little effect on the gain.



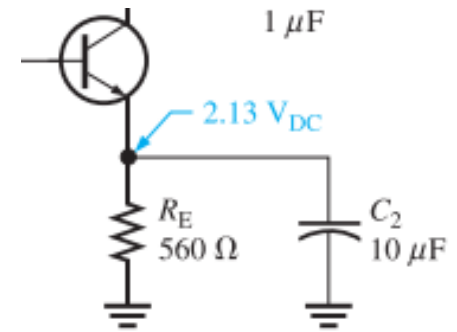
(a) Complete amplifier



(b) AC equivalent ( $X_{C1} = X_{C2} = X_{C3} = 0$ )

## Effect of the Emitter Bypass Capacitor on Voltage Gain

- ✓ The emitter bypass capacitor, which is  $C_2$  in Figure , provides an **effective short** to the ac signal around the emitter resistor, thus **keeping the emitter at ac ground**



- The value of the bypass capacitor must be **large enough** so that its reactance over the frequency range of the amplifier is very small (Ideally 0 ohms) compared to  $R_E$ .
- A good rule-of-thumb is that the capacitive reactance,  $X_C$ , of the bypass capacitor should be at least 10 times smaller than  $R_E$  at the minimum frequency for which the amplifier must operate

### EXAMPLE 6-4

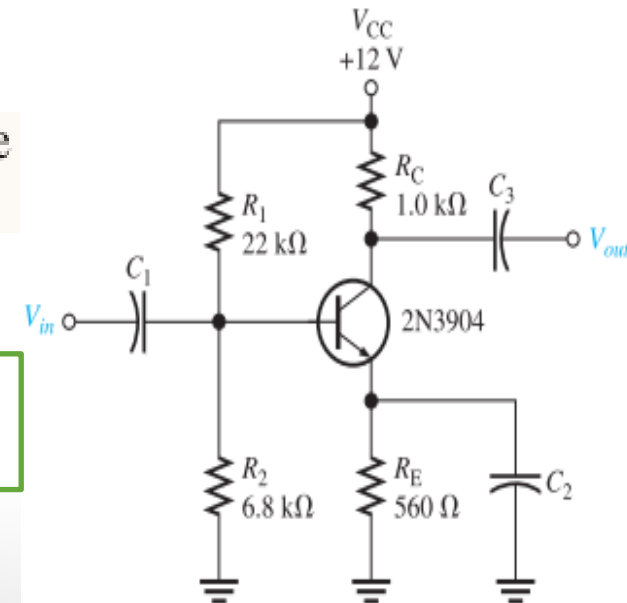
$$10X_C \leq R_E$$

Select a minimum value for the emitter bypass capacitor,  $C_2$ , in Figure 6-16 if the amplifier must operate over a frequency range from 200 Hz to 10 kHz.

$$X_{C2} = \frac{R_E}{10} = \frac{560 \Omega}{10} = 56 \Omega$$

Determine the capacitance value at the minimum frequency of 200 Hz as follows

$$C_2 = \frac{1}{2\pi f X_{C2}} = \frac{1}{2\pi(200 \text{ Hz})(56 \Omega)} = 14.2 \mu\text{F}$$



## Effect of the Emitter Bypass Capacitor on Voltage Gain

### Voltage Gain Without the Bypass Capacitor

- ✓ **Without** the bypass capacitor, the emitter is no longer at ac ground.
- ✓ Instead,  $R_E$  is seen by the ac signal between the emitter and ground and effectively adds to  $r_e'$  in the voltage gain formula and **reduces the gain**:

$$A_v = \frac{R_C}{r_e' + R_E}$$

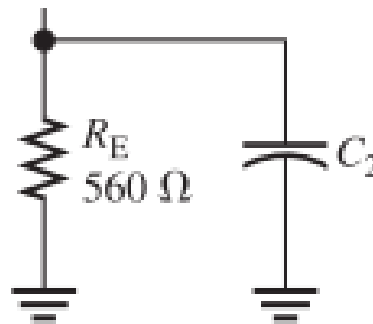
**Proof (Page 288- Boylstad)**

**EXAMPLE 6-5** Calculate the base-to-collector voltage gain of the amplifier in Figure 6-16 both without and with an emitter bypass capacitor if there is no load resistor.

$$r_e' = 6.58 \Omega$$

**Without C2, the gain is**

$$A_v = \frac{R_C}{r_e' + R_E} = \frac{1.0 \text{ k}\Omega}{567 \Omega} = 1.76$$



**With C2, the gain is**

$$A_v = \frac{R_C}{r_e'} = \frac{1.0 \text{ k}\Omega}{6.58 \Omega} = 152$$

## Stability of the Voltage Gain

- ✓ Stability is a measure of how well an amplifier maintains its design values over changes in temperature or for a transistor with a different  $B$ .
- ✓ Although bypassing  $R_E$  does produce the maximum voltage gain, there is a stability problem because the ac voltage gain is dependent on  $r_e$

$$A_v = R_C / r_e'$$

- ✓ Since  $r_e$  depends on  $I_E$  and on temperature, the gain is unstable over changes in temperature
- ✓ With no bypass capacitor, the gain is decreased because  $R_E$  is now in the ac circuit and the gain became:

$$A_v = \frac{R_C}{r_e' + R_E} \cong \frac{R_C}{R_E}$$

- **How to minimize the effect of  $r_e$  without reducing the voltage gain to its minimum value.**

**Swamping**



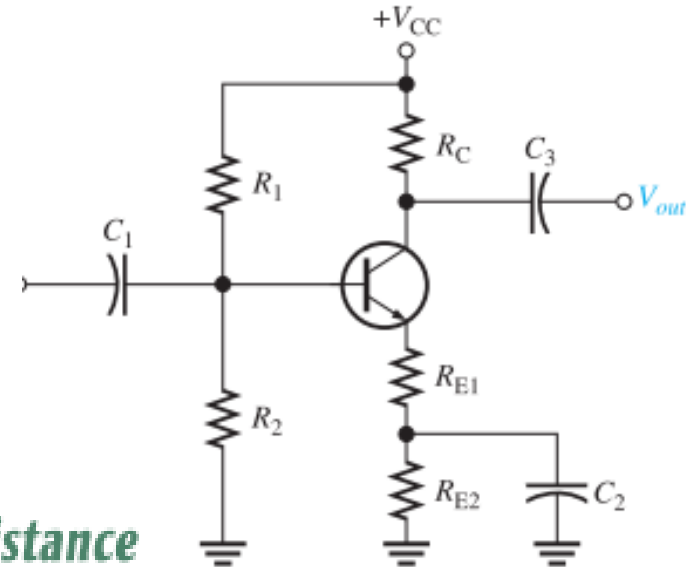
## Swamping RE effect on the Gain

- Swamping is a compromise between having a bypass capacitor across RE and having no bypass capacitor at all.
- In a swamped amplifier, RE is partially bypassed so that a reasonable gain can be achieved, and the effect of re on the gain is greatly reduced or eliminated.

$$A_v = \frac{R_C}{r'_e + R_{E1}}$$

- If RE1 is at least ten times larger than re then the effect of re is minimized and the approximate voltage gain for the swamped amplifier is:

$$A_v \cong \frac{R_C}{R_{E1}}$$

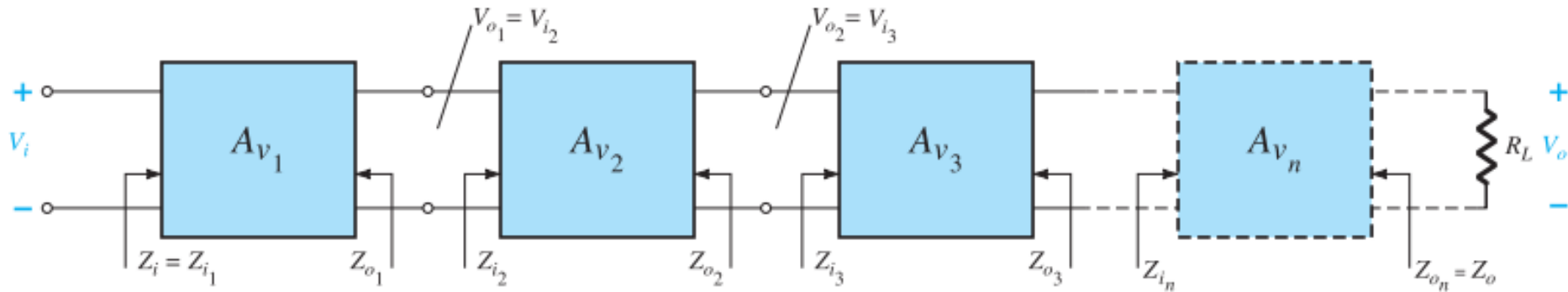


### The Effect of Swamping on the Amplifier's Input Resistance

$$R_{in(base)} = \beta_{ac}(r'_e + R_{E1})$$

# MULTISTAGE AMPLIFIERS

- Two or more amplifiers can be connected in a cascaded arrangement with the output of one amplifier driving the input of the next.
- The basic purpose of using multistage is to increase the overall voltage gain.



**FIG. 5.67**

*Cascaded system.*

$$A_{vT} = A_{v1} \cdot A_{v2} \cdot A_{v3} \cdots$$

- Amplifier voltage gain is often expressed in decibels (dB) as follows:

$$A_{v(\text{dB})} = 20 \log A_v$$

- Total gain in dB is given by:  $A'_{v(\text{dB})} = A_{v1(\text{dB})} + A_{v2(\text{dB})} + \cdots + A_{vn(\text{dB})}$

## Amplifiers Coupling

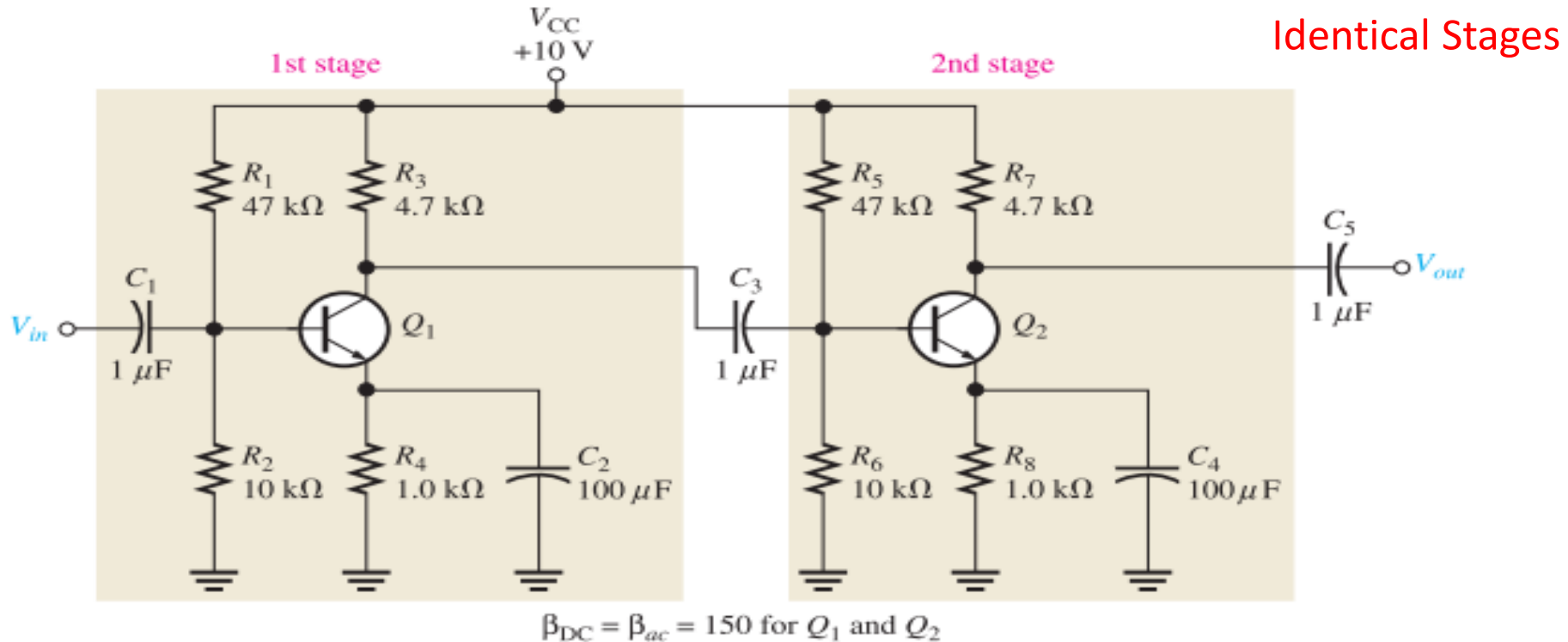
1. RC-Coupling
2. Transformer Coupling
3. Direct Coupling

The purpose of coupling device (*e.g.* a capacitor, transformer etc.) is

- (*i*) to transfer a.c. output of one stage to the input of the next stage
- (*ii*) to isolate the d.c. conditions of one stage from the next stage.

## Capacitively-Coupled (R-C Coupling)

- The output of the first stage capacitively *coupled* to the input of the 2<sup>nd</sup> stage.
- Capacitive coupling prevents the dc bias of one stage from affecting that of the other but allows the ac signal to pass without attenuation



- The first stage introduces a loading effect to the second stage.
- Because the coupling capacitor  $C_3$  effectively appears as a short at the signal frequency, the total input resistance of the second stage presents an ac load to the first stage.

DC Analysis of each stage (Identical and capacitively coupled)

$$\text{Since } \beta_{DC}R_4 \gg R_2 \quad \text{and } \beta_{DC}R_8 \gg R_6$$

the dc base voltage for  $Q_1$  and  $Q_2$  is

$$V_B \cong \left( \frac{R_2}{R_1 + R_2} \right) V_{CC} = \left( \frac{10 \text{ k}\Omega}{57 \text{ k}\Omega} \right) 10 \text{ V} = 1.75 \text{ V}$$

The dc emitter and collector voltages are as follows:

$$V_E = V_B - 0.7 \text{ V} = 1.05 \text{ V}$$

$$I_E = \frac{V_E}{R_4} = \frac{1.05 \text{ V}}{1.0 \text{ k}\Omega} = 1.05 \text{ mA}$$

$$I_C \cong I_E = 1.05 \text{ mA}$$

$$V_C = V_{CC} - I_C R_3 = 10 \text{ V} - (1.05 \text{ mA})(4.7 \text{ k}\Omega) = 5.07 \text{ V}$$

$$r'_e = 23.8 \Omega, \quad = 25 \text{ mV}/I_E$$

$$R_{in(base2)} = 3.57 \text{ k}\Omega \quad = \beta r_e$$

## Capacitively-Coupled (R-C Coupling)

- AC equivalent of first stage showing loading from second stage input resistance.

### Voltage Gain of the First Stage

The ac collector resistance of the first stage is

$$R_{c1} = R_3 \parallel R_5 \parallel R_6 \parallel R_{in(base2)}$$

$$R_{c1} = 4.7 \text{ k}\Omega \parallel 47 \text{ k}\Omega \parallel 10 \text{ k}\Omega \parallel 3.57 \text{ k}\Omega = 1.63 \text{ k}\Omega$$

$$A_{v1} = \frac{R_{c1}}{r'_e} = \frac{1.63 \text{ k}\Omega}{23.8 \Omega} = 68.5$$

### Voltage Gain of the Second Stage

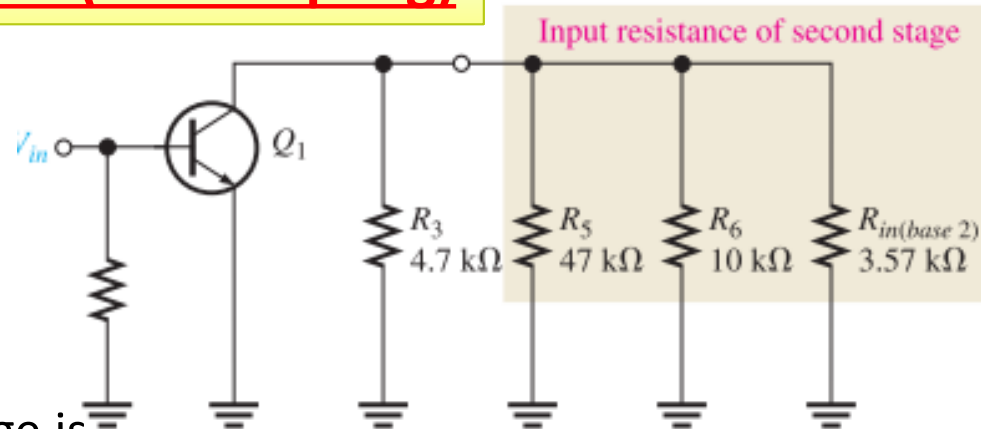
- The second stage has no load resistor, so the ac collector resistance is  $R_7$ , and the gain is

$$A_{v2} = \frac{R_7}{r'_e} = \frac{4.7 \text{ k}\Omega}{23.8 \Omega} = 197$$

- Compare this to the gain of the first stage (Identical stages), and
- Notice how much the loading from the second stage reduced the gain.

### Overall Voltage Gain

$$A'_v = A_{v1}A_{v2} = (68.5)(197) \cong 13,495$$



## Direct-Coupled Multistage Amplifiers

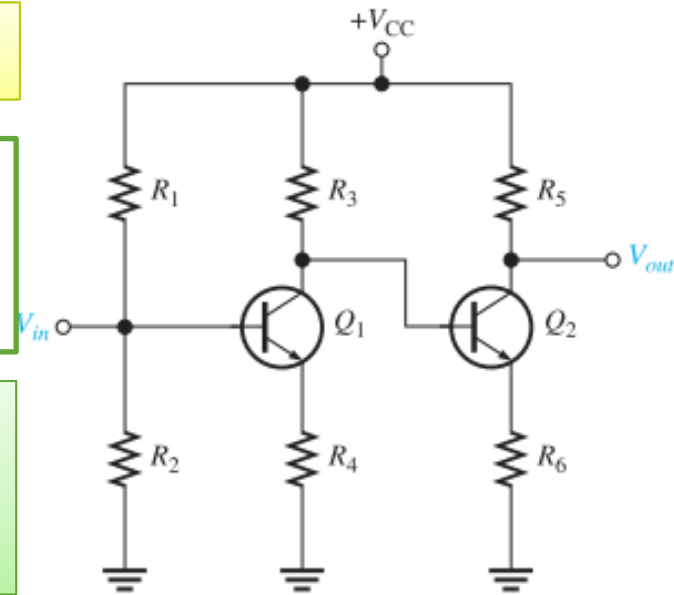
- There are no coupling or bypass capacitors
- The dc collector voltage of the first stage provides the base-bias voltage for the second stage.

- Because of the direct coupling, this type of amplifier has a **better low-frequency response** than the **capacitively coupled type**

- At Low Frequencies:
  - ✓ The reactance of coupling and bypass capacitors may become excessive.
  - ✓ The increased reactance of capacitors produces gain reduction in capacitively coupled amplifiers.

- Direct-coupled amplifiers can be used to amplify low frequencies all the way down to dc (0 Hz) without loss of voltage (no capacitors)

- The disadvantage of direct-coupled amplifiers, is that small changes in the dc bias voltages from temperature effects or power-supply variation are amplified by the succeeding stages, which can result in a significant drift in the dc levels throughout the circuit.



## Next Lecture

- Amplifiers Classes (A, B, AB, and C)